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2001 1988

## Using Granger Test in the Analysis of Stationary Time series

### Abstract

In this research the relation among rain , temperature and relative humidity in Mosul city of the time 1988-2001 was determined by applying Granger test to determine and measure the direction of the causative relation among the variables of the research. To make clear whether the chain is stable or not there

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was a need for using units root test to check the characters of time chains of the sample variables to know the extent of their stability and determining the degree of integrity of each variable alone. The results showed that the variables were highly integrated so , due to that the joint integrity test was used to determine he existence or the absence of the longterm relation among the variables under the study. The analysis showed the absence of the joint integrity among the variables of the research, besides the instability of remains of the joint integrity equation .Also , passage analysis was used to show the causative relation among the variables under the study and this test boosted by results we came up with by applying Granger test.

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Granger

1974

Newbold

t

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**Co – integration concept and Theorem statistic Granger**  
Granger (1969)

. (2008 ) .

. (1994 ) .

Engle – Granger

((1987)

$d$   $y_t$   
 $I (d)$   $d$

$y_t \sim I (1)$

(  $\Delta y_t$  )  $\Delta y_t \sim I(0)$

(Sahabethin : 2007)

$\beta$   $y_t , x_t$

...

$$y_t = \alpha + \beta x_t + U_t \dots(1)$$

:

:  $y_t$

:  $x_t$

$$u_t \sim (0, \sigma^2 u)$$

:  $u_t$

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$y_t \ x_t$

(Equilibrium error)

. (2007 ) .

**(Granger Causality test)**

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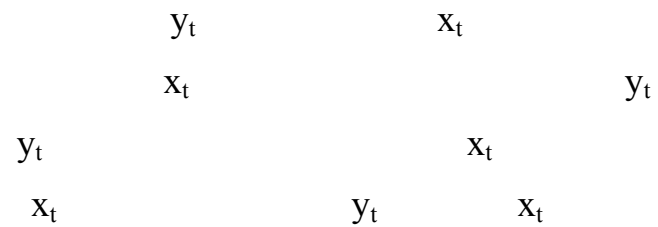
(

( )

(2005 )

:

(Granger, 1969)



$y_t$

(Greene , 2000) .

(Granger Casuatty)

F

$$F = \frac{(SSR_r - SSR_u) / m}{SSR_u / (n - k_u)} \dots (2)$$

$$H_0 : \sum_{i=1}^n \alpha_i = 0$$

$$H_1 : \sum_{i=1}^n \alpha_i \neq 0$$

F (m,n-k<sub>u</sub>)

F

)

: SSR<sub>R</sub>

(

( )

: SSR<sub>u</sub>

: K<sub>u</sub>

: m

: n

F

F

(x<sub>t</sub>

y<sub>t</sub>

y<sub>t</sub>

x<sub>t</sub>

(Gujaratee , 1995)

### Path Analysis

(Causal models)

. effect      Cause  
Sewell   Wright

(r)

. (effect)	(cause)	direct effect	-
	Indirect effect		-
) . (other causes)		(paths)	

(1987)

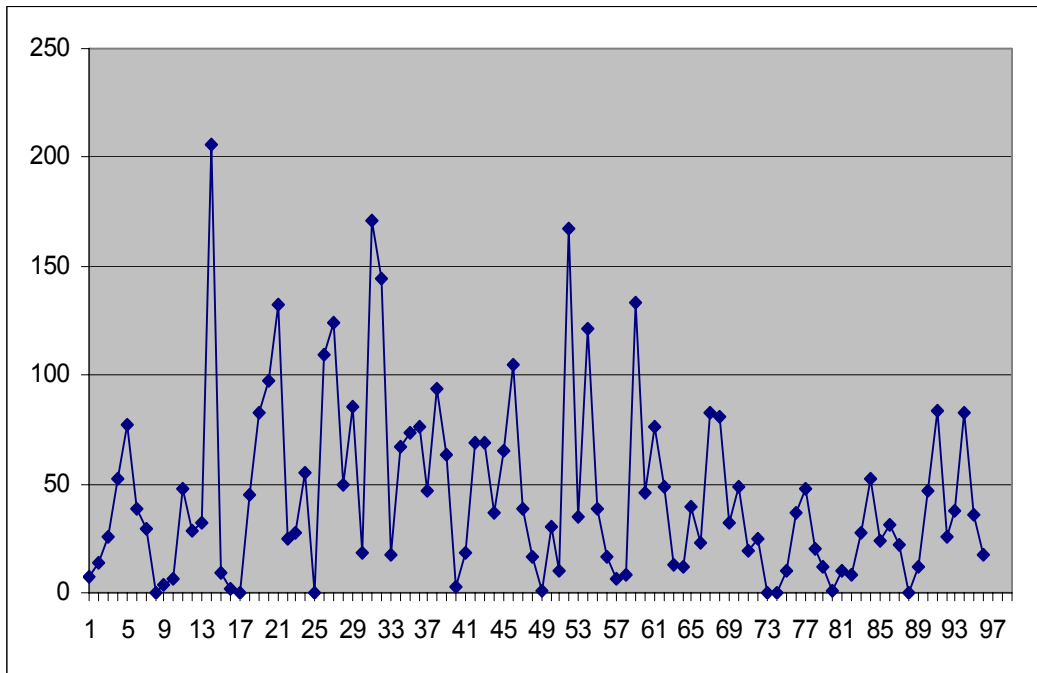
(      )

96

2001

1988

(1)



( 1 )

-1988

2001

(1)

. (unit root tests)

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(Dickey and Fuller , 1979)

( Phillip perron : 1988)

(1)

Augmented Dickey – fuller (ADF) and (DF) unit root tests

<b>-2.158822</b>	<b>-1.46519</b>	<b>-1.02544</b>	<b>13.5997</b>	<b>11.0257</b>	<b>13.8011</b>	

(ADF)

t

(1)

Stationary

(non-stationary)

(first difference)

(2007 ) .

$$t\left(\frac{\alpha}{2}, n - 2\right) = t\left(\frac{0.05}{2}, 96 - 2\right) \quad (0.025, 94 = 1.99)$$

(ADF) 1.99

t

11.0257

13.8011

(ADF)

t

13.5997

t

(ADF)

-1.02599

(ADF)

- 2.15882

- 1.046519



(2)

Phillip-perron (pp) ( unit root test)

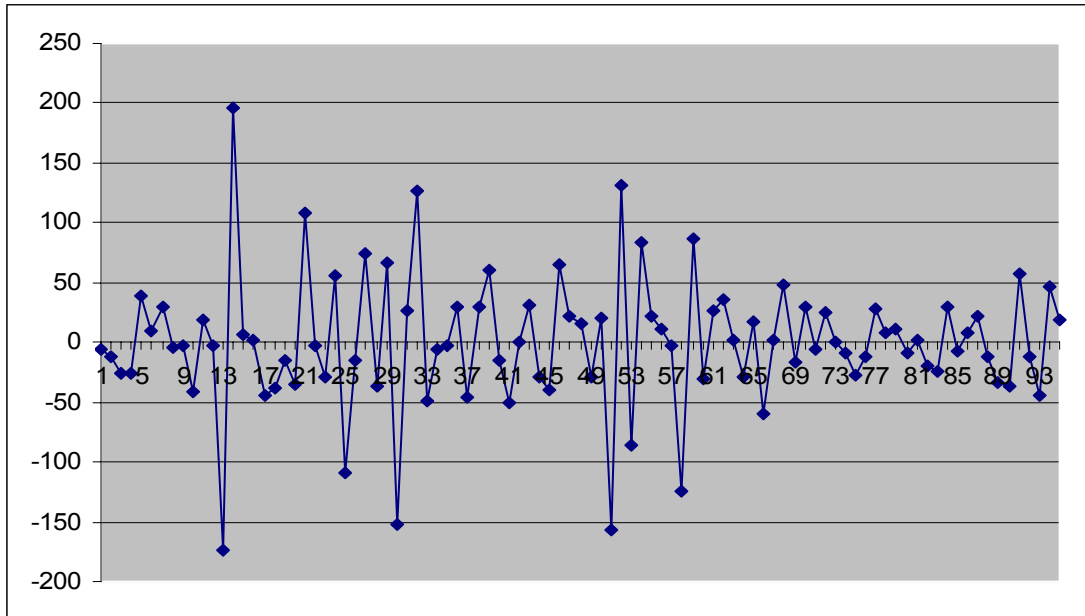
-5.30074	-6.01768	-5.30074	48.8679	55.5800	48.8679	

pp ) t (2) (1)  
 55.5800 48.8679 (test  
 ( ) ( ) 48.8679

-6.01768

-5.30074

-5.30074



: (2)

( Granger Causahty test )

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.(Eviews 5)

F 3.96 F 10.9816 F .  
 F  
 . 0.07032 F  
 F 9.63125 F

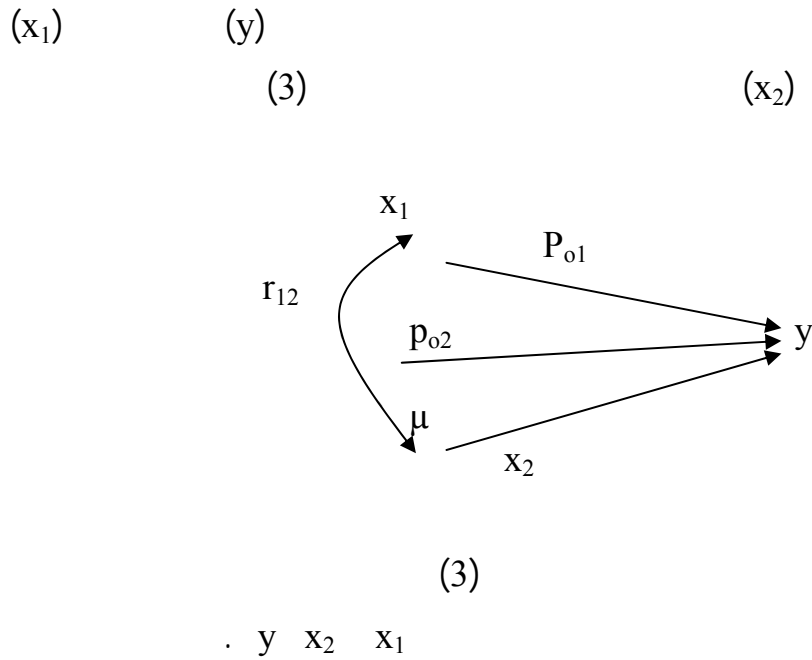
( 3 )

Pairwise Granger Causality Tests  
 Sample: 1 96  
 Lags: 2

Probability	F-Statistic	Obs	Null Hypothesis:
5.5E-05	10.9816	94	SERIES02 does not Granger Cause SERIES01
0.93215	0.07032		SERIES01 does not Granger Cause SERIES02
0.00016	9.63125	94	SERIES03 does not Granger Cause SERIES01
0.81592	0.20391		SERIES01 does not Granger Cause SERIES03
0.45013	0.80543	94	SERIES03 does not Granger Cause SERIES02
1.0E-05	13.1304		SERIES02 does not Granger Cause SERIES03

0.80543 F  
 F  
 F 13.1304

**path Analysis**



$$r_{10} = -0.44662129 \quad r_{12} = 0.976225$$

$$r_{20} = -0.47546$$

$$.(p_{02}) y \quad x_2 \quad (p_{01}) y \quad x_1$$

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$$\begin{pmatrix} r_{11} & r_{12} \\ r_{21} & r_{22} \end{pmatrix} \begin{pmatrix} p_{01} \\ p_{02} \end{pmatrix} = \begin{pmatrix} r_{10} \\ r_{20} \end{pmatrix}$$

: P  
: r  
y

RP = r

$$\begin{bmatrix} r_{11} & r_{12} \\ r_{21} & r_{22} \end{bmatrix} \begin{bmatrix} p_{01} \\ p_{02} \end{bmatrix} = \begin{bmatrix} r_{10} \\ r_{20} \end{bmatrix}$$

$$\begin{bmatrix} 1 & 0.976225 \\ 0.976225 & 1 \\ -0.44662129 & \\ -0.47546 & \end{bmatrix} \begin{bmatrix} p_{01} \\ p_{02} \end{bmatrix} =$$

P = R<sup>-1</sup> r

$$\begin{bmatrix} p_{01} \\ p_{02} \end{bmatrix} = \begin{bmatrix} 1 & 0.976225 \\ 0.976225 & 1 \end{bmatrix}^{-1} \begin{bmatrix} -0.44662129 \\ -0.47546 \end{bmatrix}$$

$$R^{-1} = \begin{bmatrix} 21.2835 & -20.7775 \\ -20.7775 & 21.2835 \end{bmatrix} \begin{bmatrix} -0.44662129 \\ 0.47546 \end{bmatrix}$$

$$\begin{bmatrix} p_{01} \\ p_{02} \end{bmatrix} = \begin{bmatrix} 0.371980 \\ -0.838536 \end{bmatrix}$$

y (degree of determination) R<sup>2</sup>

R<sup>2</sup><sub>O(12)</sub>

x<sub>2</sub> x<sub>1</sub>

$$R^2_{O(12)} = p_{01} r_{10} + p_{02} r_{20} =$$

$$(0.371980)(-0.44662129) + (-0.838536)(-0.47546)$$

$$= (-0.0746412) + (0.3986903) = 0.3240491$$

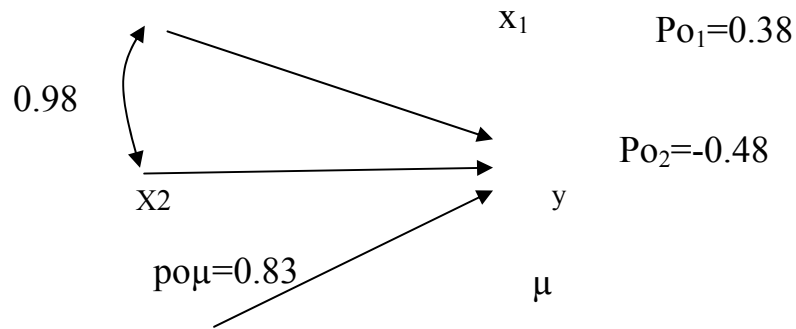
$$x_2 \quad x_1 \quad y$$

$$R^2_{o(12)} = 0.3240491$$

$$R^2_{o(12)} + P^2_{o\mu} = 1$$

$$\therefore p^2_{om} = 1 - R^2_{o(12)} = 1 - 0.3240491 = 0.6759509$$

$$\therefore P^2_{o\mu} = \sqrt{P^2_{o\mu}} = \sqrt{0.6759509} = 0.8221623$$



$$y \quad x_2 \quad y \quad x_1$$

(4)

y x <sub>2</sub> , x <sub>1</sub> : (4)	
Coefficient	
0.371980	y x <sub>1</sub> -1 p <sub>01</sub> = .
-0.818599	r <sub>12</sub> p <sub>02</sub> = x <sub>2</sub>
-0.4466191	r <sub>10</sub> =
-0.838536	y (x <sub>2</sub> ) -2 p <sub>02</sub> = .
0.3631361	r <sub>12</sub> p <sub>01</sub> = x <sub>1</sub>
-0.4753999	r <sub>20</sub> =

: (4)

x<sub>1</sub>

x<sub>2</sub>

$$0.371980$$

$$-1.1305184$$

$$+ = x_1$$

$$-0.4466191 = 0.371980 + (-0.818599)$$

$$\cdot y \quad x_1$$

$$x_2 \quad -2$$

$$(p_{02}) -0.838536$$

$$r_{12} p_{01} = 0.3631361 \quad x_1$$

$$+ = x_2$$

$$r_{02} \quad -0.4753999 = 0.3631361 + (-0.838536) =$$

**(Co-integration test)**

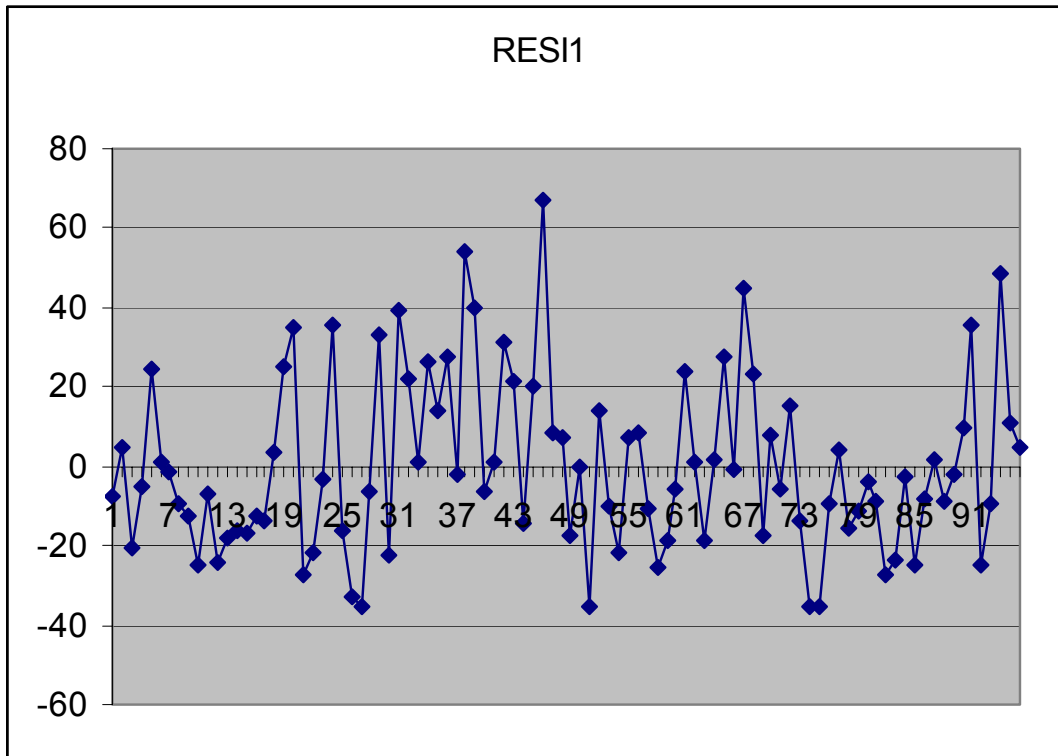
non-)

(Engle and Granger:1987)

(stationary

$$y = 25.9 + 1.31x_1 - 2.10x_2 \dots (3)$$

(3)



(6)

(6)

(3)

(5)

(ADF test)

:(5)

(PP test)

PP	ADF	PP	ADF	PP	ADF	
47.8678	13.8011	48.58679	13.5997	55.5800	11.02577	



(5)

1.99 t (3)

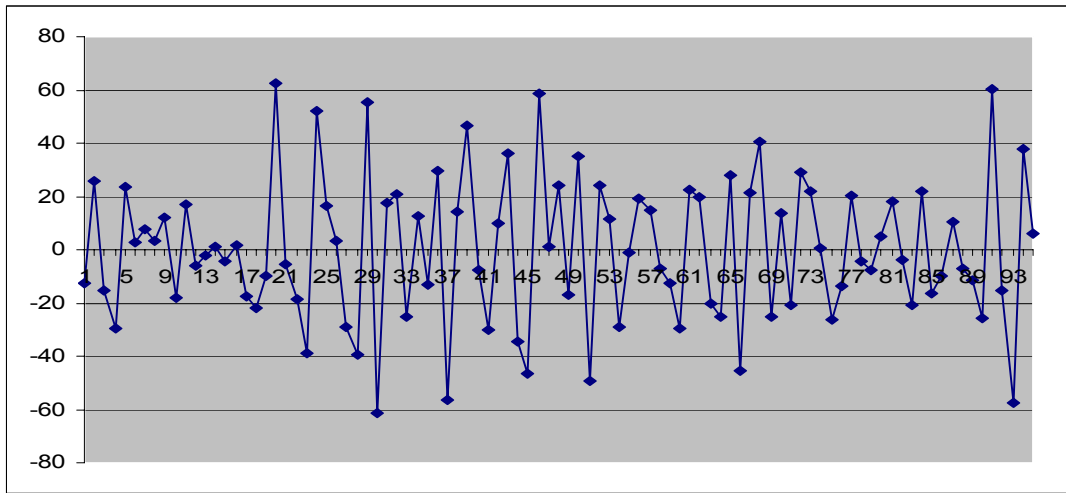
13.5997 13.8011 (ADF)

11.02577

:

(pp 1.96 t (pp test)

. 0.05 test)



:(7)

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.2001 -1988

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.2

.3

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1. " ( 2005 )  
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  2. " ( 1987 )  
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  3. " : ( 2007 )  
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  4. " : ( 2004 )  
" . 32
  5. " ( 2008 )  
"
  6. " : ( 1994 )  
" . 24-22
- . ( 44 )

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23.6	15.9	27.2
29	21.6	55.4
30.5	21.4	0
17.7	12.9	109
15.1	6.8	124
11.4	5.8	49.8
13.1	7.55	85.9
18.6	11.2	18.8
23.1	16.7	171
27.9	21.1	144
30.6	21.4	17.1
19	11.9	66.7
10.6	10.2	73.1
14.9	9.9	76.5
14.7	9	47.3
19.5	13.3	93.8
27.1	19.6	63.7
33.8	24.4	2.9
30.3	22.7	18.2
20.5	14.2	68.6
15.3	6.15	68.6
13.6	8.55	37.2
16.5	10.4	65.7
20.2	13.5	105
23.7	17	39
33.9	24.7	16.5
29.8	21.1	0.7

2001-1988

درجة الحرارة	الرطوبة النسبية	الامطار
31.2	22.4	7.3
24.4	14.2	134
15.9	8.05	25.8
10.7	5.6	52.4
13	8.3	77.5
20.3	13.4	38.6
23.4	16.6	29.7
33.6	24	0.3
30.4	22.3	4
23.5	16.1	6.2
12.4	9.45	47.9
13.1	7.3	28.5
14.2	7.8	32
18.6	13.2	206
26.1	18.7	9
31.5	23	2.1
31.6	22.6	0.2
19	15.5	44.6
11.1	7.9	82.6
8.3	3.9	97.8
9.7	5.65	133
16	9.45	24.6

27.4	19.4	11.7
36.1	27.2	1.2
29.4	23.3	10.5
21.4	14.2	8.2
13.9	10.1	28
12	7.2	52.6
15.1	8.7	23.7
19.3	11.7	31.1
28.5	21.1	22.3
34.1	25.7	0.3
31.4	21.2	12.4
20.6	14.2	46.7
15.2	9.5	83.7
14.1	8.55	25.9
15.8	9.95	37.9
22.2	15.9	82.5
26.2	18.5	36.2
32.3	23.7	17.6

23.4	12.9	30.2
16.4	7.75	10.1
13.1	8.5	167
16.8	11	34.9
17.7	12.8	122
23.3	16.8	38.7
34.5	25.8	16.5
30.2	21.1	6.1
21.9	15.1	8.7
14.1	11.8	133
13.7	8.35	45.6
13.3	6.8	75.9
15.6	9.95	48.7
23.3	16.1	12.9
33.8	24.5	11.5
32.3	22.6	39.9
26.4	15	23.3
19.5	9.25	83
10.8	6.6	81.1
14.4	8.35	32.6
18.9	12.7	48.5
26.3	18.7	19.5
33.8	24.6	24.8
31.8	22.8	0.1
21.8	18.1	0.1
16.8	12	9.7
16.2	10	36.8
17.3	10.8	48.2
21.2	13.5	19.8